

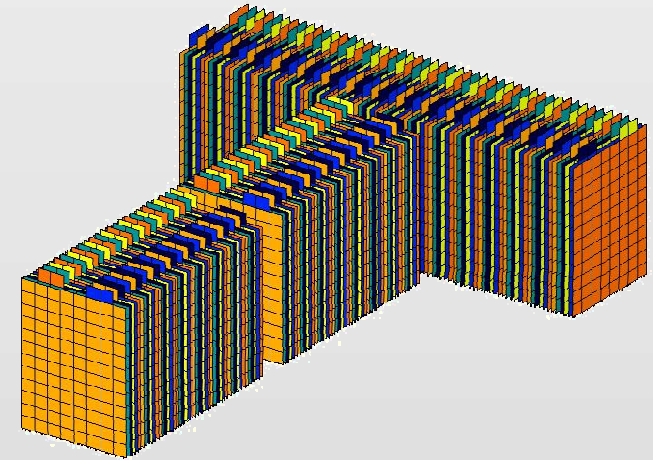


ThermoAnalytics[®]
Total Thermal Solutions

RadTherm Battery Modeling UGM 2011- Antti Jussila

Agenda

- Battery Design Issues
- Physical Description
- Model Description
 - Approach
 - Implementation
- Model Inputs
- Development Status



RadTherm Battery Simulation

■ 1D System Tools

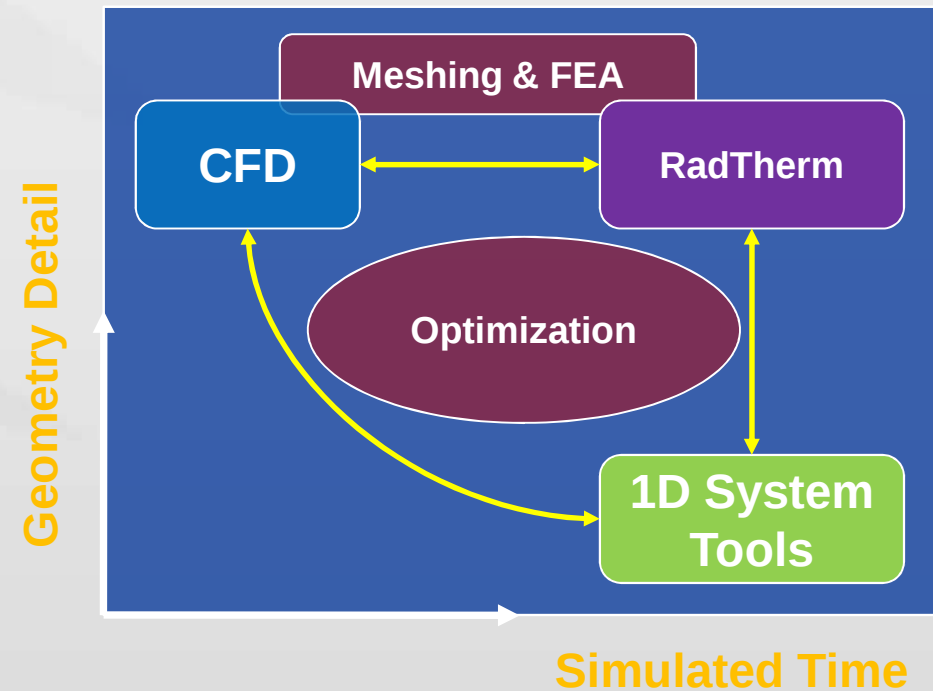
- Concept 1D Component Models
- Long Transients solved quickly

■ RadTherm

- Simple 1D, 2D or Detailed 3D Geometry
- Radiation, Conduction, Convection
- Long Transient
- Rapid Trade Studies

■ CFD

- Highly Detailed 3D Geometry
- Complex Flow
- Steady State or Short Transient



CAE Coupling & Integration

1D Tools – AMESim, Matlab, ...

CFD – Fluent, PowerFLOW, STAR-CCM+, ...

Optimization – Isight, modeFRONTIER, ...

Meshing – ANSA, Hypermesh, PowerDELTA,

FEA – ABAQUS, NASTRAN

Thermal Issues

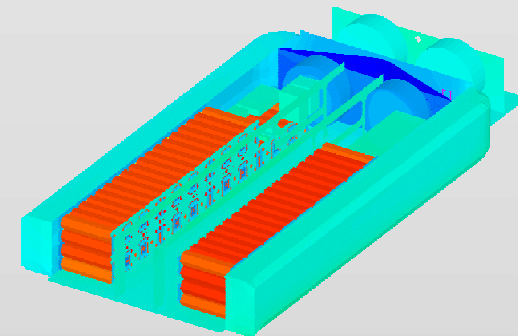
- Battery Cells, Packs & Systems

- Cells – uniform current, temperature distribution
- Packs – uniform cooling, environmental effects
- Systems – Cell balance, SOC estimation



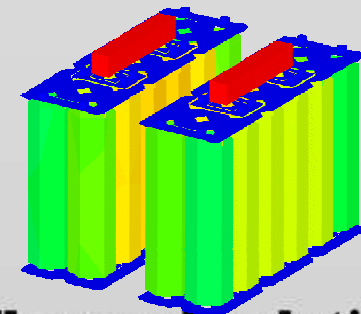
- Cooling Strategies

- Air (dedicated or shared)
- Liquid (dedicated or shared)
- Heat sink, cooling plates, heat pipe,



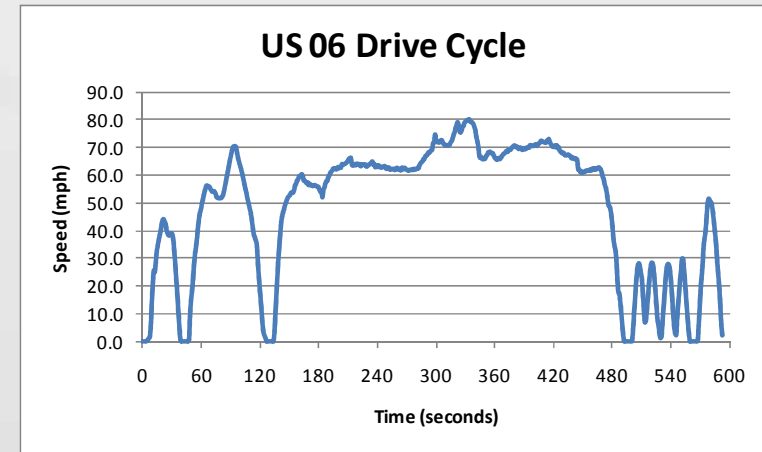
- Hybrid & Electric Vehicle Batteries

- Performance
- Lifetime & Durability
- Safety



Thermal Scenarios

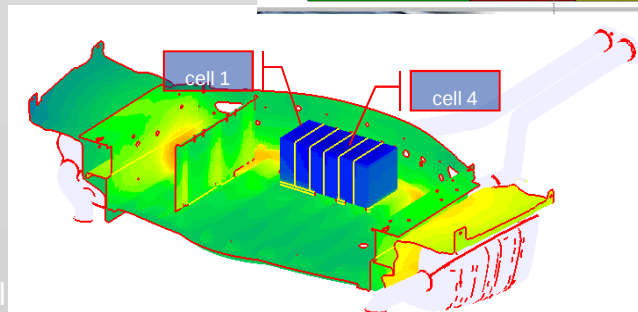
- Transient
 - Drive Cycles
 - Hot Soak
 - Preheating for Cold Start
 - Load Balancing
 - Abuse Tolerance
 - Cooling System Faults
 - Thermal Runaway



Hill climb with trailer

Three phases:
- Conditioning
- Load
- Soak

The aim is to mimic the physical test procedure and produce the same results using RadTherm.



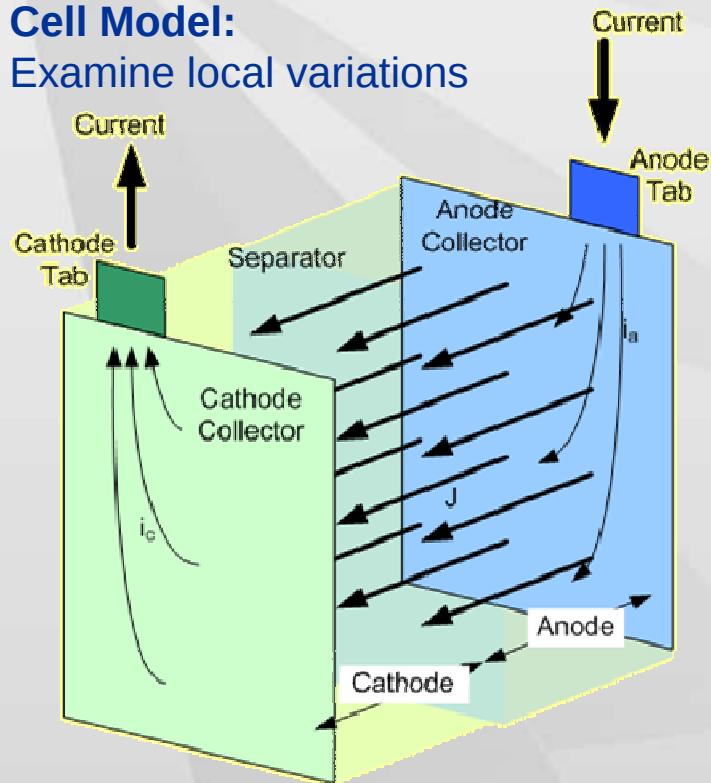
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Battery Modeling Description

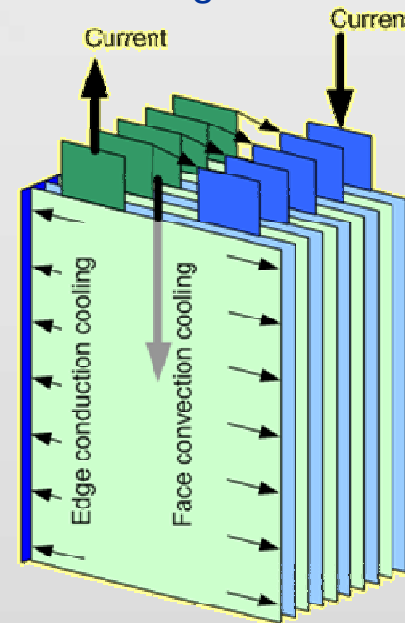
Cell Model:

Examine local variations



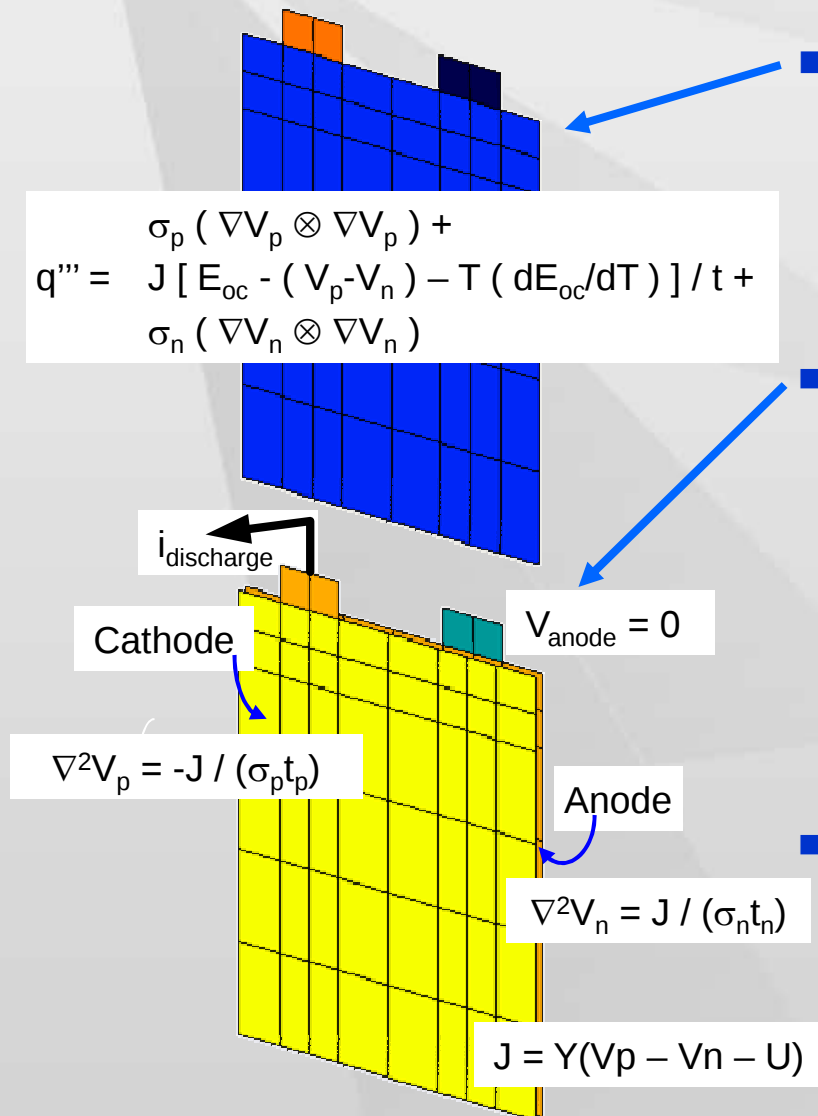
- Effects of tab size/location, cell size, collector thickness:
 - Voltage gradients on collector plates
 - Non-uniform current density
 - Non-uniform ion depletion
 - Non-uniform heating
- Electrical load

Pack Model: examine variations in cell-to-cell average behavior



- Effects of pack configuration, flow distribution, packaging:
 - Non-uniform cell behavior
 - Non-uniform cooling
- Effects of electrical load on total thermal load
 - Charge/discharge profile

Battery Model Implemented in RadTherm



■ Thermal problem

- Description of temperature distribution on electrodes

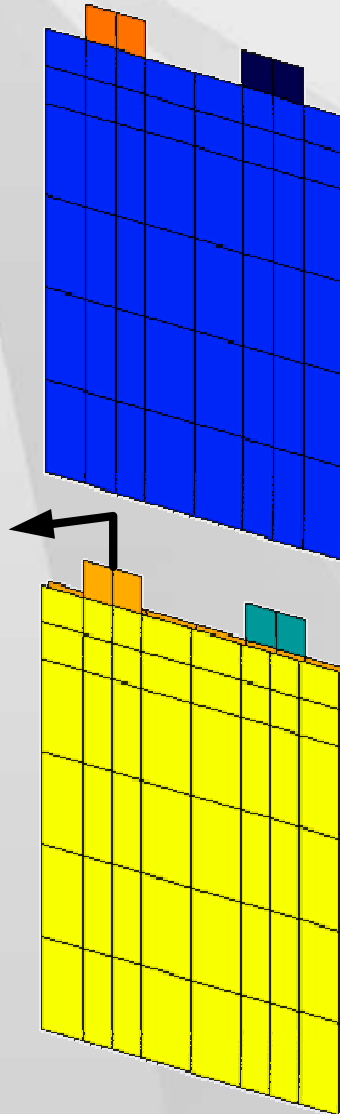
■ Electrical problem

- Description of current density through electrodes
- Description of voltage distribution on collector plates
- RadTherm solves thermal analog:
 - Thermal Conductivity = Electrical Conductivity
 - Temperature = Voltage
 - Heat Flux = Current Density

■ Two problems coupled via joule heating

- Calculated in Electrical
- Imposed on Thermal

Battery Model Setup in RadTherm



■ Thermal problem

- Cell modeled as multi-layer part
 - Thermal properties of electrodes
 - Convection on front, back face
 - Optional edge conduction
 - Hook function imposes Joule heating derived from electrical model

■ Electrical problem

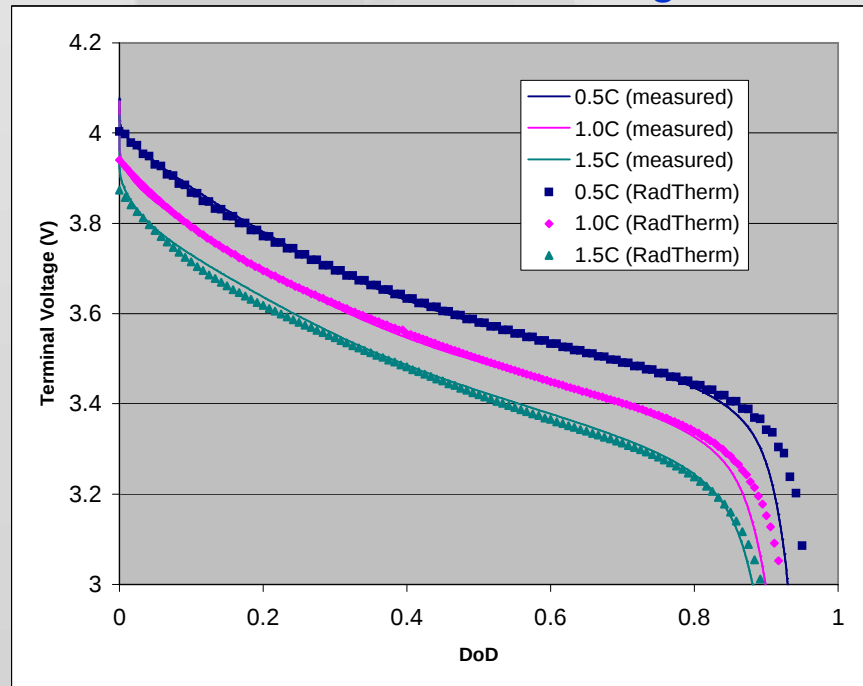
- Anode, cathode collector plates modeled as standard parts
 - k = electrical conductivity
 - Hook function imposes a 'heat flux' equivalent to the current density between electrodes
 - Anode tab is assigned a value of 0 volts (ref voltage)
 - 'Heat' equal to discharge current is imposed on cathode tab
 - 'Temperature' solution is voltage distribution
- ## ■ So far, coupling is only one-way
- Electrical affects thermal
 - Future development will add two-way coupling

Battery Cell Model Validation

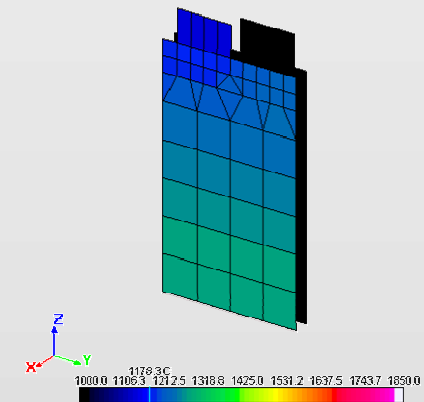
Cell data

Time (sec)	DoDAvg	Cathode Voltage (mV)	Anode Voltage (mV)	Cell Current Density (A/m ²)	Uniformity Index
0	0	4.05E+03	-6.10E-06	-5.38E+02	0
60	0.016	4.03E+03	-6.10E-06	-5.24E+02	0.068
120	0.032	4.00E+03	-6.10E-06	-5.37E+02	0.057
180	0.048	3.98E+03	-6.10E-06	-5.25E+02	0.048
240	0.064	3.95E+03	-6.10E-06	-5.36E+02	0.042
300	0.08	3.93E+03	-6.10E-06	-5.26E+02	0.037
360	0.096	3.91E+03	-6.10E-06	-5.36E+02	0.033
420	0.113	3.89E+03	-6.10E-06	-5.27E+02	0.03

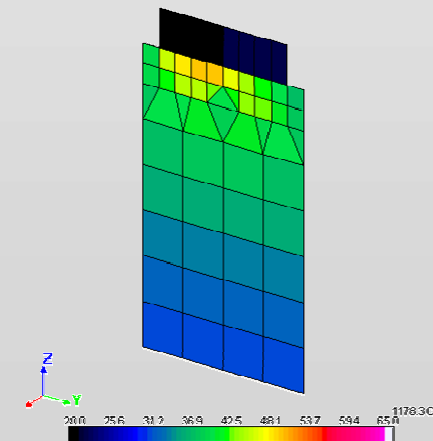
Measured & Simulated discharge curves



2D Voltage Distribution

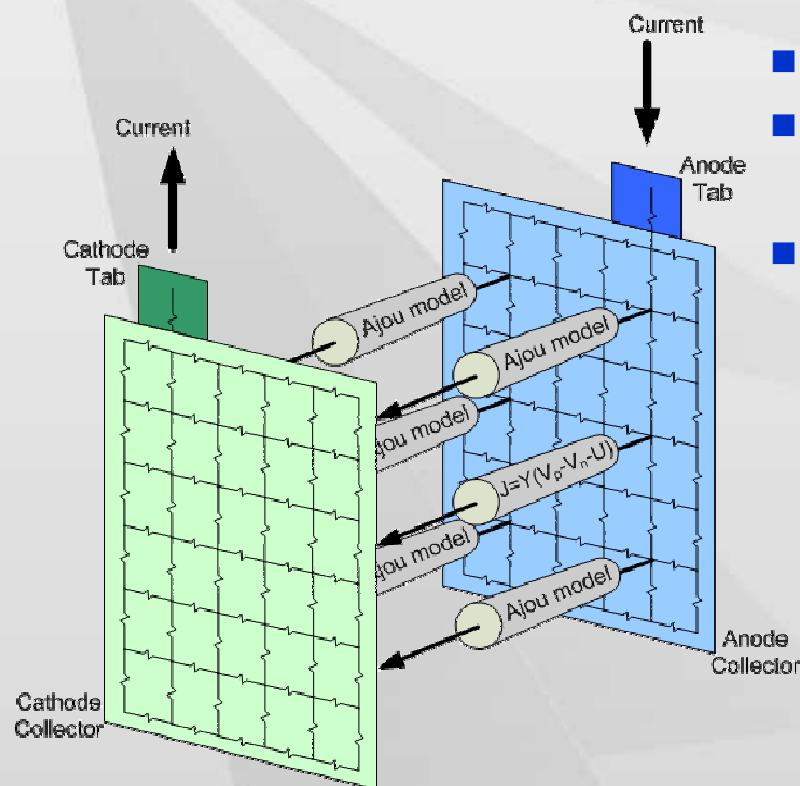


2D Temperature Distribution



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Ajou Model* Provides Current Density Through Electrodes as Function of Voltage Difference



- Empirical model
- Current Density through Electrodes
- Local current density = function of local potential difference across cell
 - $J = Y (V_p - V_n - U)$
 - V_p = potential on cathode
 - V_n = potential on anode
 - U = fitting parameter ($\approx$ open cell voltage)
 - $U = \sum a_i \text{DoD}^i$; $i=0,1,2,\dots$
 - Y = effective conductivity of cell
 - $Y = \sum b_i \text{DoD}^i$; $i=0,1,2,\dots$
 - DoD = Depth of Discharge
 - $\text{DoD} = \int J dt / Q_T$
 - Q_T = theoretical capacity per unit area
 - DoD varies across electrode area

* Also known as NTG model

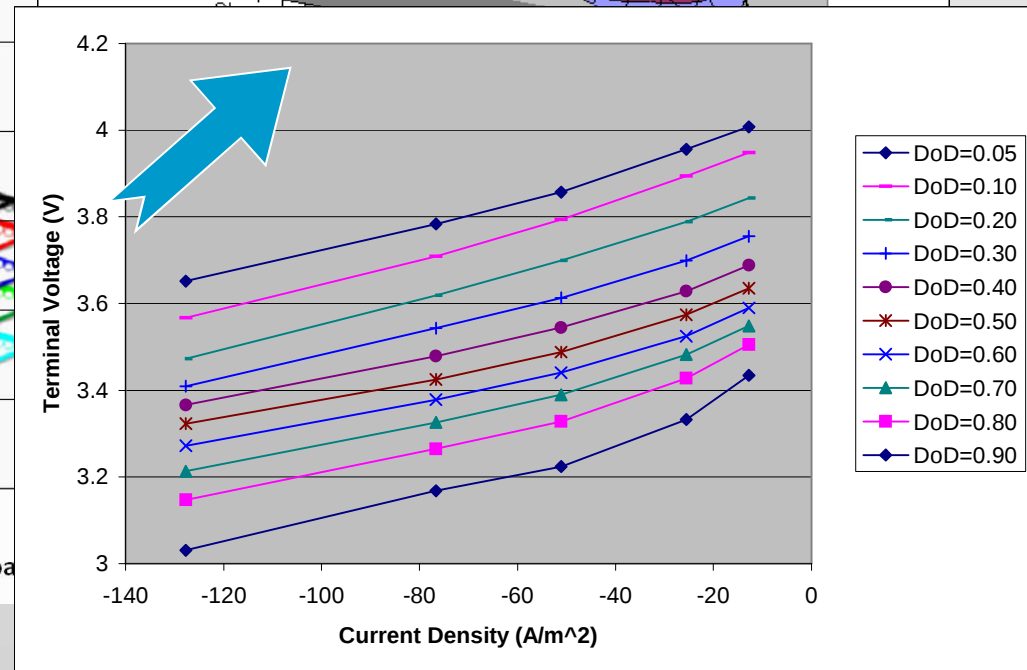
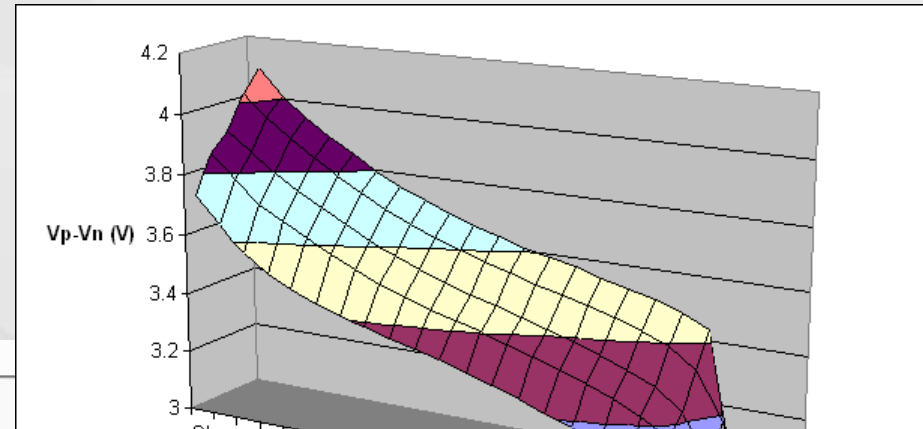
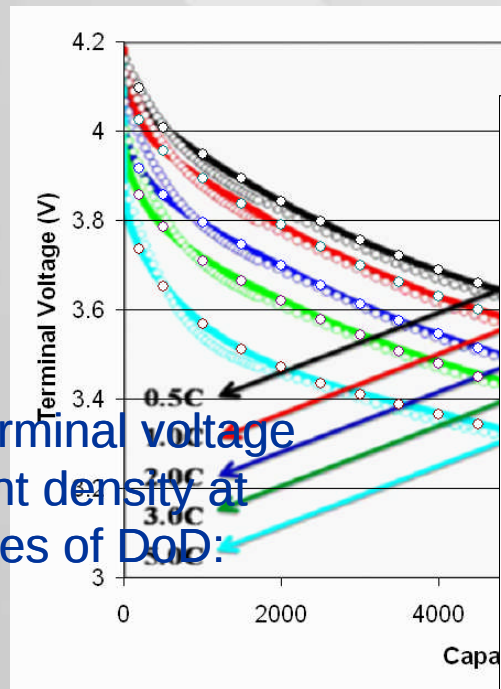
Required Battery Test data

- Data needed to calculate Ajou coefficients
 - Theoretical cell capacity
 - Electrode area
 - Discharge current – 1c, 2c, 4c
 - Voltage data during discharge, correlated to discharge current
 - sufficient to resolve curve at beginning of discharge, end of discharge

Battery Discharge Data to Coefficients

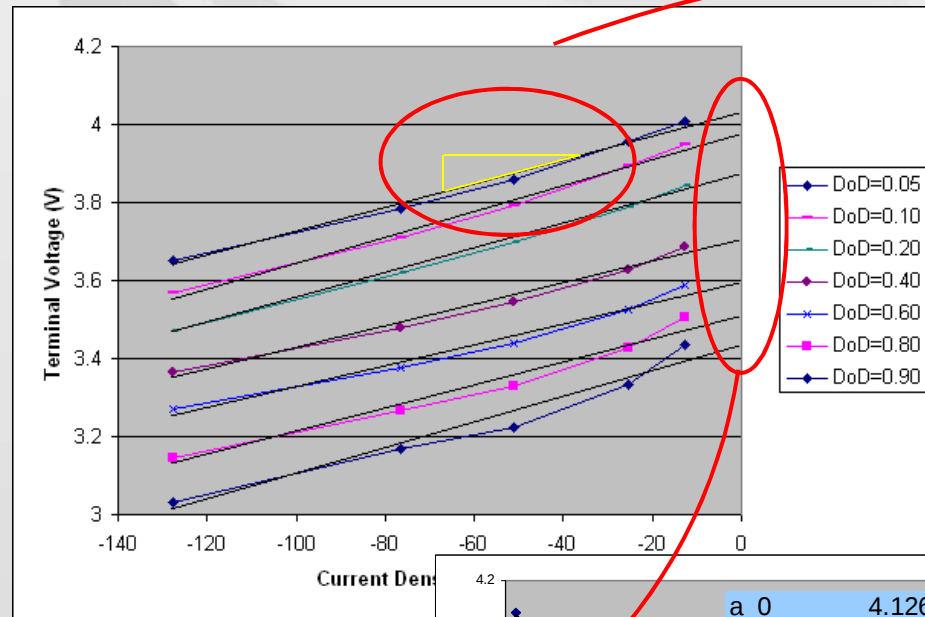
Obtain terminal voltage versus DoD at different values of current density:

Cross-plot terminal voltage versus current density at different values of DoD:



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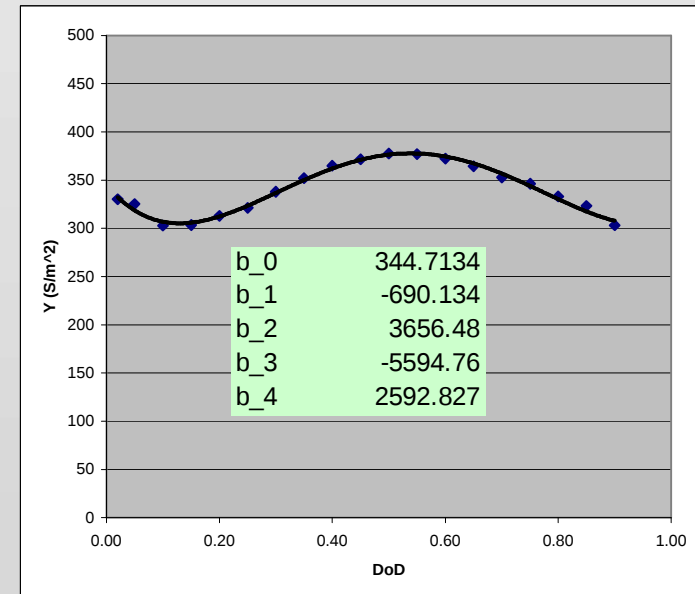
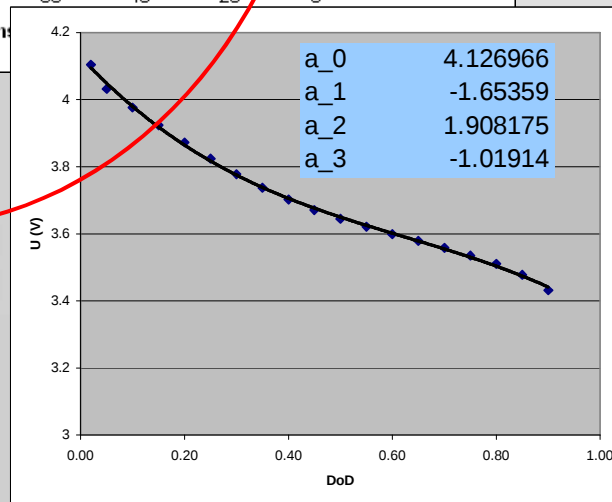
U and Y determined from line fits to data



Slope of line is $1/Y$

DoD	Y
0.02	330.1501
0.1	302.8415
0.2	312.8386
0.4	364.8562
0.6	372.4626
0.8	333.1441
0.9	303.0941

DoD	U
0.02	4.104145
0.1	3.976391
0.2	3.872191
0.4	3.702418
0.6	3.59893
0.8	3.510945
0.9	3.431629



$$Y = 344.7 - 690.1\text{DoD} + 3656\text{DoD}^2 - 5595\text{DoD}^3 + 2593\text{DoD}^4$$

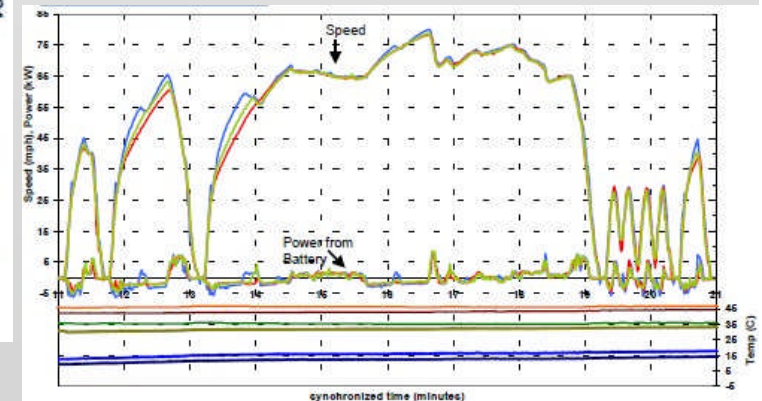
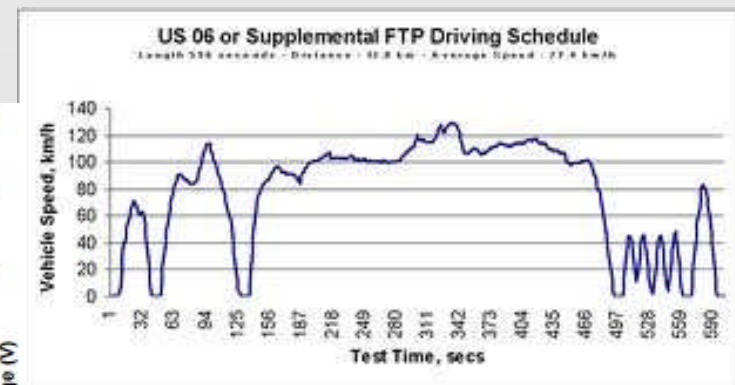
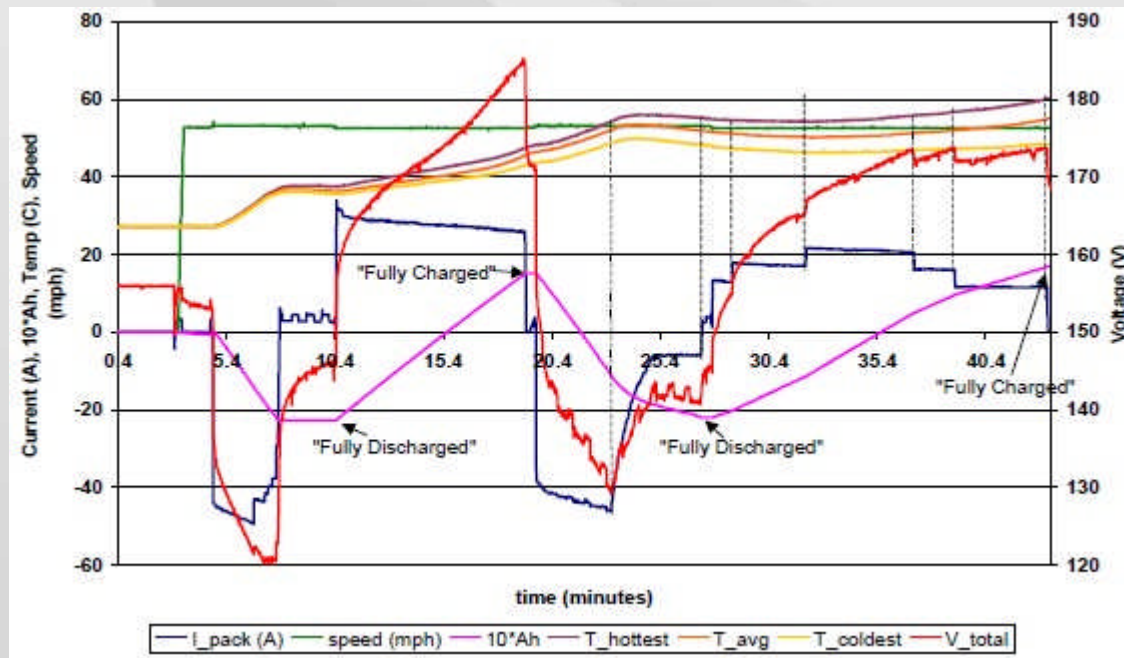
Intercept of line is U

$$U = 4.127 - 1.654\text{DoD} + 1.908\text{DoD}^2 - 1.0193\text{DoD}^3$$

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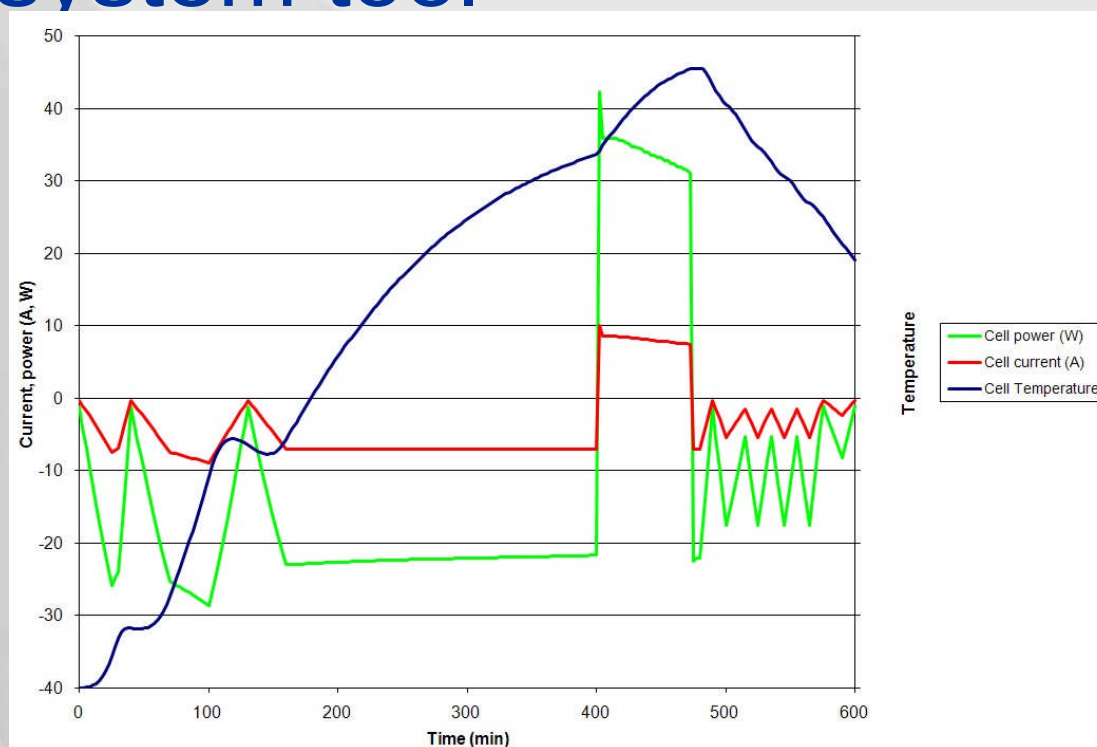
Next Steps-Drive Cycle - US06

■ Transient Current and Voltage inputs



Transient data input-demo example

- Data input from Excel spreadsheet or 1D system tool



- Current input, Temperature output